

Electrical Level 4



Advanced Controls 26407-14



Objectives

When trainees have completed this lesson, they should be able to do the following:

1. Select and install solid-state relays for specific applications in motor control circuits.
2. Install non-programmable/programmable motor circuit protectors (solid-state overload relays) in accordance with the manufacturer's instructions.
3. Select and install electromechanical and solid-state timing relays for specific applications in motor control circuits.
4. Recognize the different types of reduced-voltage starting motor controllers and describe their operating principles.



Objectives and Performance Task

5. Connect and program adjustable frequency drives to control a motor in accordance with the manufacturer's instructions.
6. Demonstrate and/or describe the special precautions used when handling and working with solid-state motor controls.
7. Recognize common types of motor braking and explain the operating principles of motor brakes.
8. Perform preventive maintenance and troubleshooting tasks in motor control circuits.

Performance Task

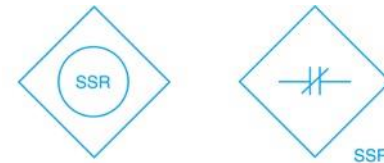
Identify and connect various control devices.



1.0.0 – 2.6.0

Introduction; Solid-State Relays

- Solid-state relays (SSRs) have many advantages over electromechanical relays, including faster switching and superior service life, reliability, and shock/vibration resistance.
- An SSR is activated by an AC or DC voltage applied to its input terminals. DC inputs are normally less than 32VDC and applied from digitally controlled motor inputs.

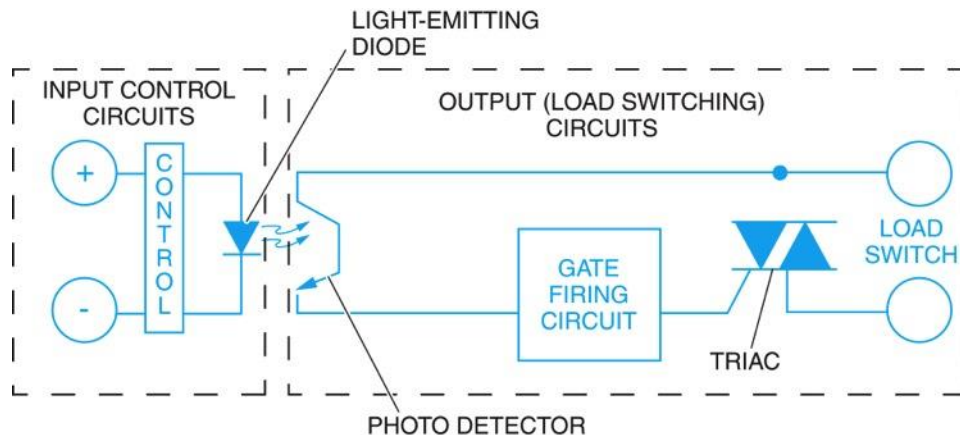


SCHEMATIC SYMBOLS



Block Diagram of an Optically Isolated Solid-State Relay

- An SSR consists of an input control circuit and an output control circuit.
- The input control circuit senses the input control signal and provides coupling between the input and output circuits using a light-emitting diode (LED) and photo detector.



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1.0.0 – 2.6.0

Comparison Chart for EMR and SSR Technology

Comparable or Equivalent Terminology for Electromechanical and Solid-State Relays	
Electromechanical Relays (EMRs)	Solid-State Relays (SSRs)
1. <i>Coil voltage</i> : The minimum voltage necessary to energize or operate the relay. This value is also referred to as the pickup voltage.	1. <i>Control voltage</i> : The minimum voltage required to gate or activate the control circuit of the solid-state relay. Generally a maximum value is also specified.
2. <i>Coil current</i> : In conjunction with the coil voltage, the amount of current necessary to energize or operate the relay.	2. <i>Control current</i> : The minimum current required to turn on the solid-state control circuit. Generally a maximum value is also specified.
3. <i>Hold current</i> : The minimum current required to keep a relay energized or operating.	3. <i>See control current</i> .
4. <i>Dropout voltage</i> : The maximum voltage at which the relay is no longer energized.	4. <i>See control voltage</i> .
5. <i>Pull-in time</i> : The amount of time required to operate (open or close) the relay contacts after the coil voltage is applied.	5. <i>Turn-on time</i> : The elapsed time between the application of the control voltage and the application of the voltage to the load circuit.
6. <i>Dropout time</i> : The amount of time required for the relay contacts to return to their normal unoperated position after the coil voltage is removed.	6. <i>Turn-off time</i> : The elapsed time between the removal of the control voltage and the removal of the voltage from the load circuit.
7. <i>Contact voltage rating</i> : Maximum voltage rating that the contacts of a relay are capable of switching safely.	7. <i>Load voltage</i> : The maximum output voltage handling capability of a solid-state relay.
8. <i>Contact current rating</i> : Maximum current rating that the contacts of a relay are capable of switching safely.	8. <i>Load current</i> : The maximum output current handling capability of a solid-state relay.
9. <i>Surge current</i> : Maximum peak current that the contacts of a relay can withstand for short periods of time without damage.	9. <i>Surge current</i> : Maximum peak current that a solid-state relay can withstand for short periods of time without damage.
10. <i>Contact voltage drop</i> : Voltage drop across relay contacts when relay is operating (usually quite low).	10. <i>Switch-on voltage drop</i> : Voltage drop across a solid-state relay when operating.
11. <i>Insulation resistance</i> : Amount of resistance measured across relay contacts in open position.	11. <i>Switch-off resistance</i> : Amount of resistance measured across a solid-state relay when turned off.
12. <i>No equivalent</i> .	12. <i>Off state current leakage</i> : Amount of current leakage through a solid-state relay when turned off but still connected to the load voltage.
13. <i>No equivalent</i> .	13. <i>Zero current turn-off</i> : Turn-off at essentially the zero crossing of the load current that flows through an SSR. A thyristor will turn off only when the current falls below the minimum holding current. If input control is removed when the current is at a higher value, turn-off will be delayed until the next zero current crossing.
14. <i>No equivalent</i> .	14. <i>Zero voltage turn-on</i> : Initial turn-on occurs at a point near zero crossing of the AC line voltage. If input control is applied when the line voltage is at a higher value, initial turn-on will be delayed until the next zero crossing.



EMR and SSR Performance

Plus (+) indicates advantages; minus (-) indicates disadvantages.

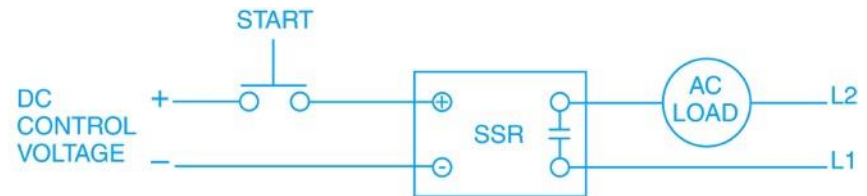
Advantages and Disadvantages of Electromechanical and Solid-State Relays		
General Characteristics	EMR	SSR
1. Arcless switching of the load	-	+
2. Electronic (IC, etc.) compatibility for interfacing	-	+
3. Effects of temperature	+	-
4. Shock and vibration resistant	-	+
5. Immunity to improper functioning because of transients	+	-
6. Radio frequency switching	+	-
7. Zero voltage turn-on	-	+
8. Acoustic noise	-	+
9. Selection of multipole, multithrow switching capability	+	-
10. Contact bouncing	-	+
11. Ability to stand surge currents	+	-
12. Response time	-	+
13. Voltage drop in load circuit	+	-
14. AC & DC switching with same contacts	+	-
15. Zero current turn-off	-	+
16. Leakage current	+	-
17. Minimum current turn-on	+	-
18. Life expectancy	-	+
19. Initial cost	+	-
20. Real cost-lifetime	-	+



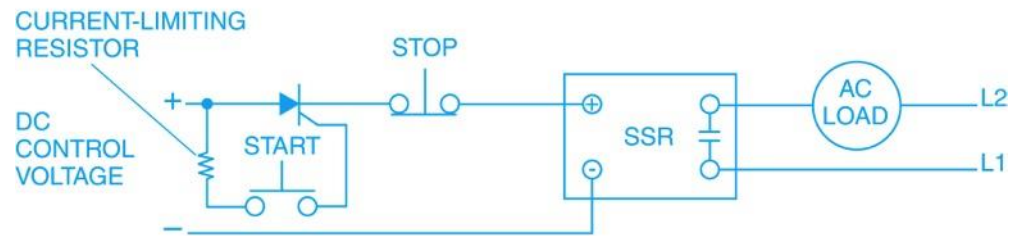
1.0.0 – 2.6.0

Two-Wire and Three-Wire SSR Control

- SSRs can be connected for either two-wire or three-wire control.
- In the two-wire circuit shown here, the SSR activates the load for as long as the Start pushbutton is pressed. In the three-wire circuit, the SSR activates a gate that maintains current flow when the pushbutton is released.



(A) TWO-WIRE CONTROL



(B) THREE-WIRE CONTROL

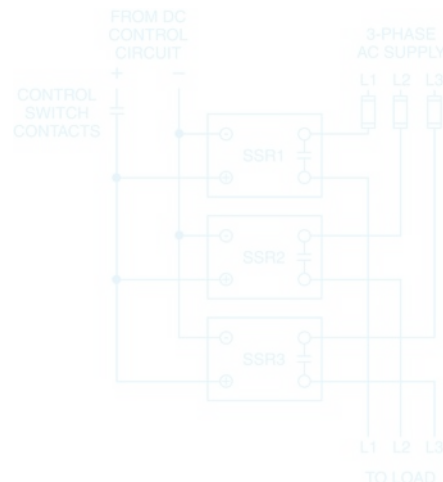
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1.0.0 – 2.6.0

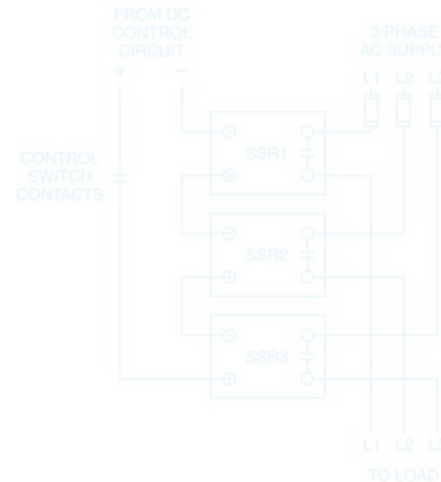
Next Session... Multiple SSRs Connected in Parallel and Series to Control a Three-Phase Load

- A single SSR can be designed for multiple switched outputs or the inputs of two or more single-output SSRs can be series- or parallel-connected to obtain the desired outputs.
- In the circuits shown here, three SSRs are controlled by a single switch to

Solid-State Protective Relays



(A) THREE SSRs CONNECTED IN PARALLEL

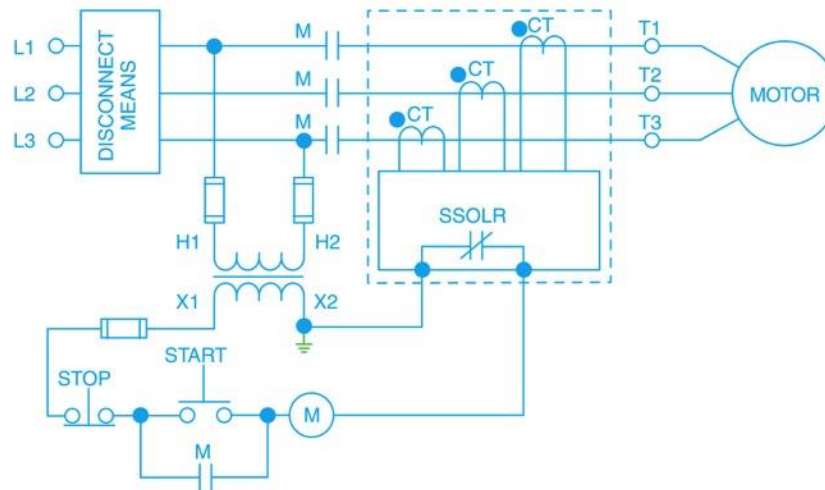


(B) THREE SSRs CONNECTED IN SERIES

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3.0.0 – 3.2.0

Solid-State Protective Relays



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3.0.0 – 3.2.0

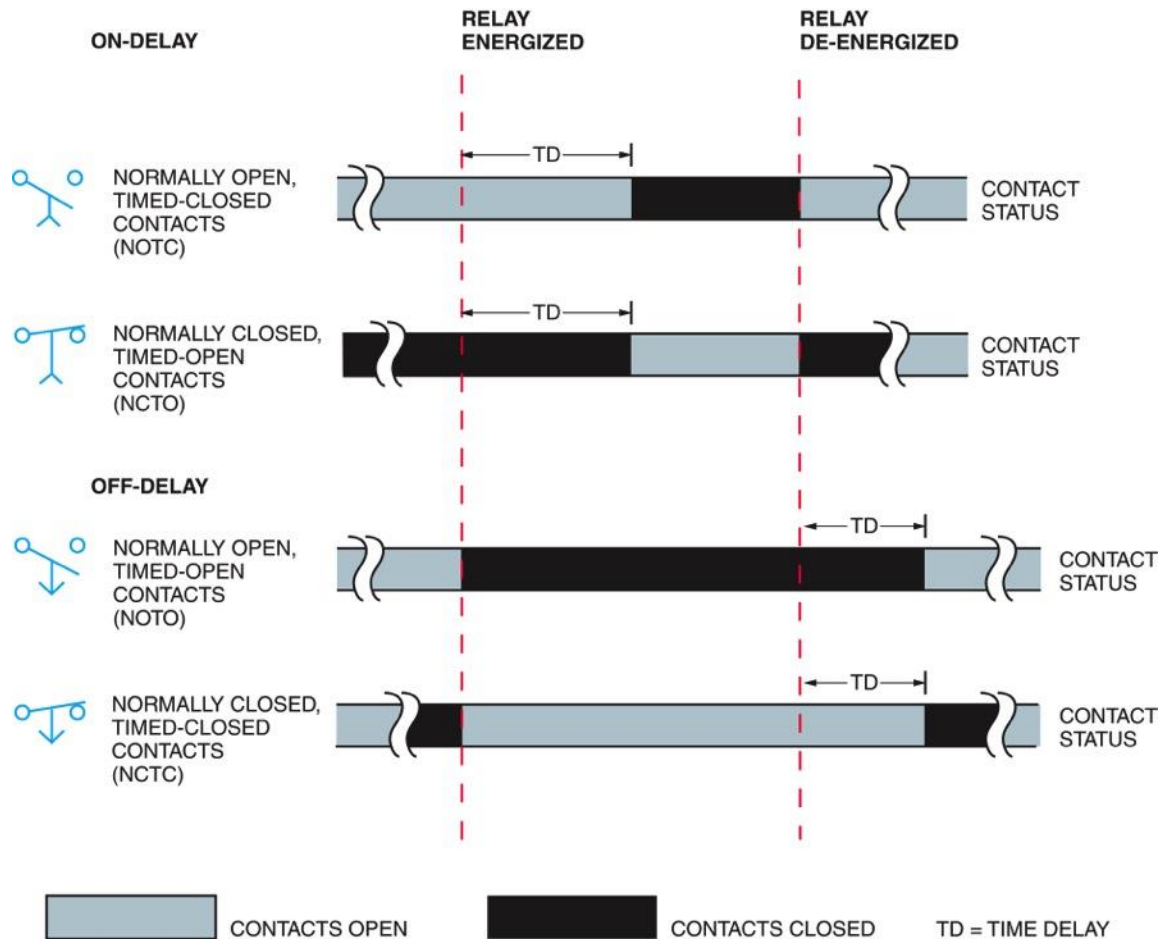
Typical Programmable Solid-State Overload Relay

- SSOLR programming is usually done using the front panel controls on the unit. Some units can be controlled using a personal computer (PC) connected via a communications network.
- The control parameters typically include various trip points and delay times. Refer to the manufacturer's instructions for the relay in use.



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Timing Relays



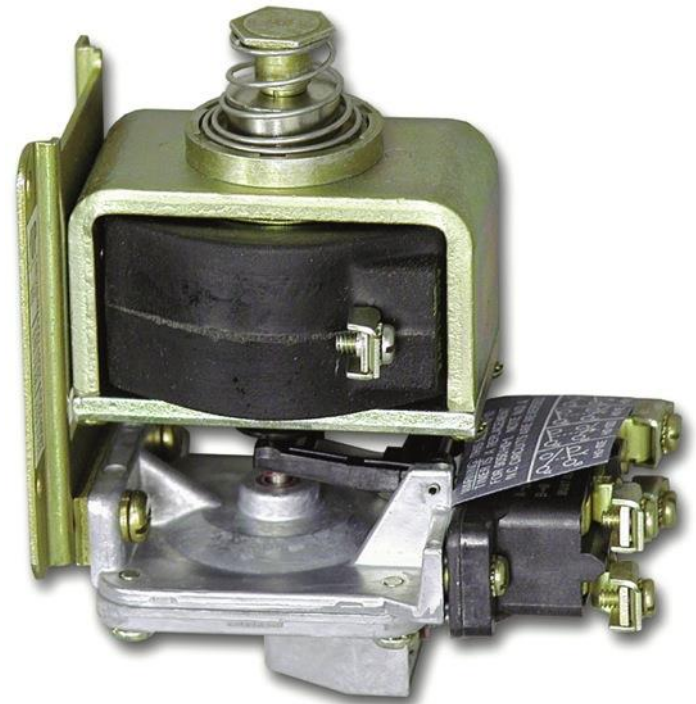
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4.0.0 – 4.4.0

Pneumatic Time Delay Relay

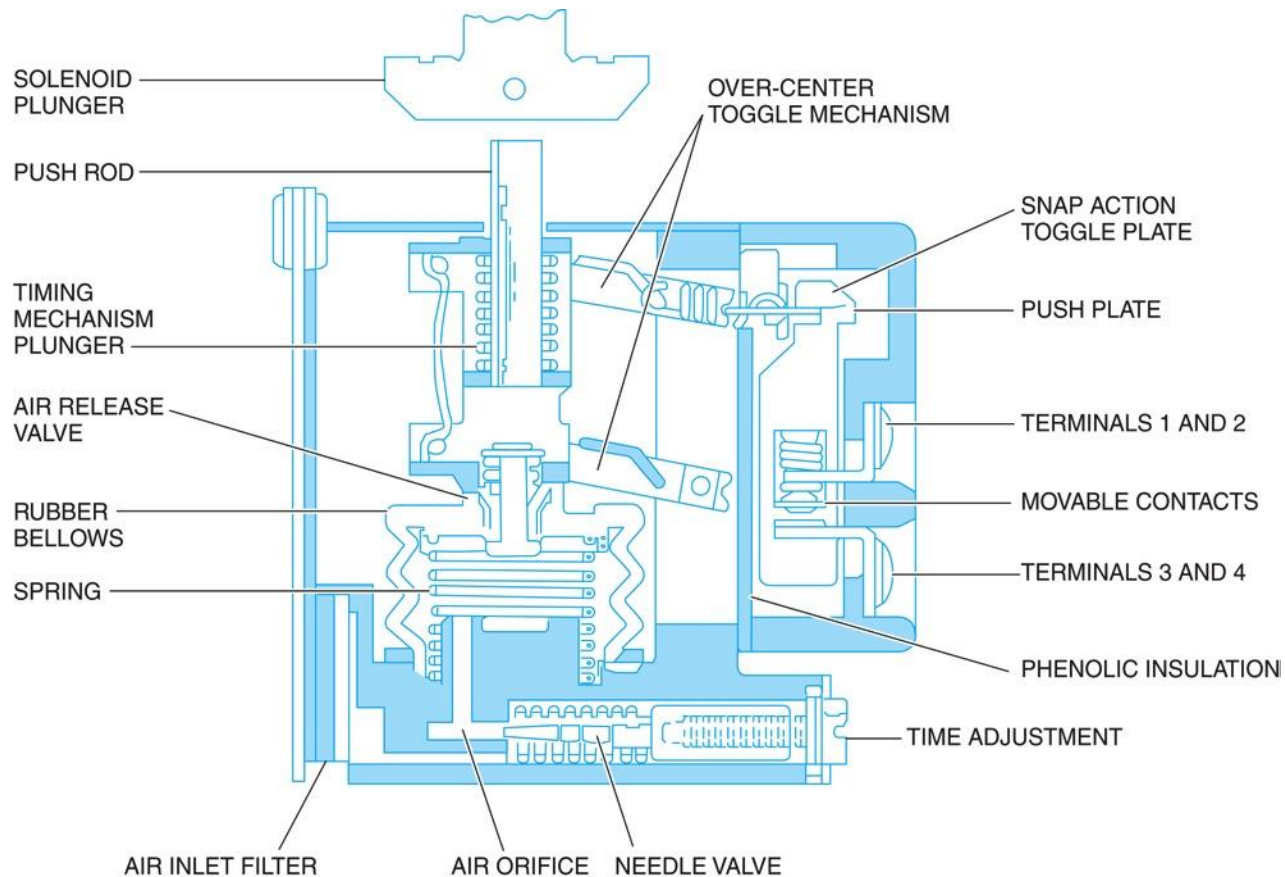
- Pneumatic timing relays are electromechanical relays that use air power to retard the movement of the relay contacts.
- The pneumatic relay shown here has one normally open (NO) contact and one normally closed (NC) contact.



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4.0.0 – 4.4.0

Cutaway View of Pneumatic Relay Contact Unit and Timing Mechanism



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4.0.0 – 4.4.0

Typical Solid-State Plug-In Timing Relay

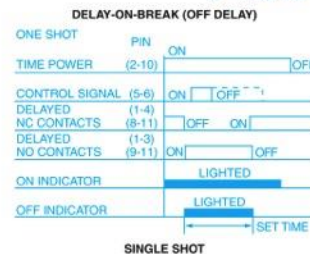
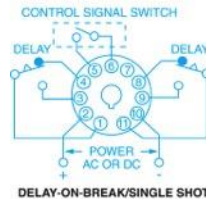
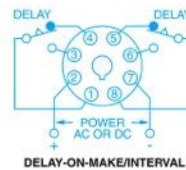
- Solid-state timing relays are used where high repeat accuracy is required and the time delay must be frequently changed.
- The solid-state timing relay shown here can provide several fixed timing ranges that are selected using controls on the top of the relay.



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4.0.0 – 4.4.0

Plug-In Solid-State Relay Connection Diagrams and Operation Charts



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4.0.0 – 4.4.0

Next Session... Starting for Three Motors

- The timing relay shown here is used to provide the staggered start of three motors on the same circuit to avoid the large inrush current that would occur if all three were to be energized at once.
- This relay provides a time delay of 20 seconds between motor starts.

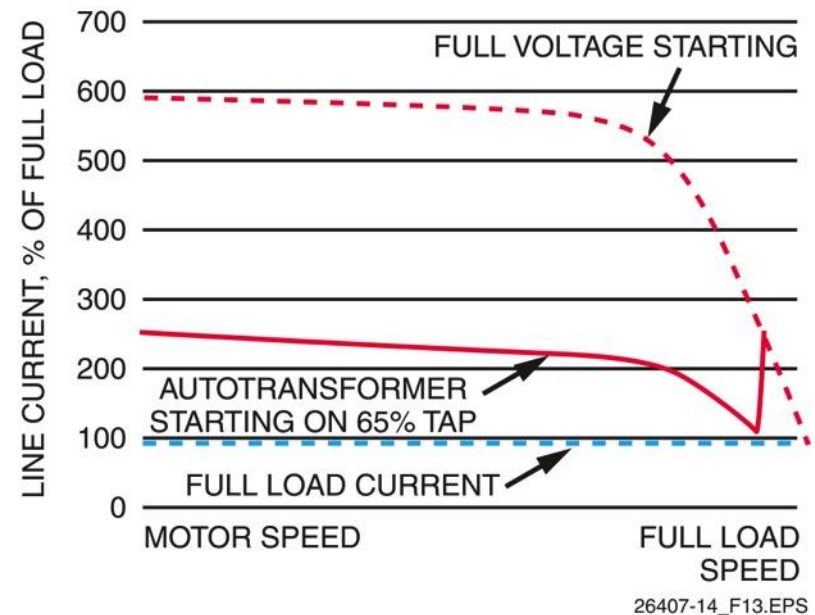


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5.0.0 – 5.5.0

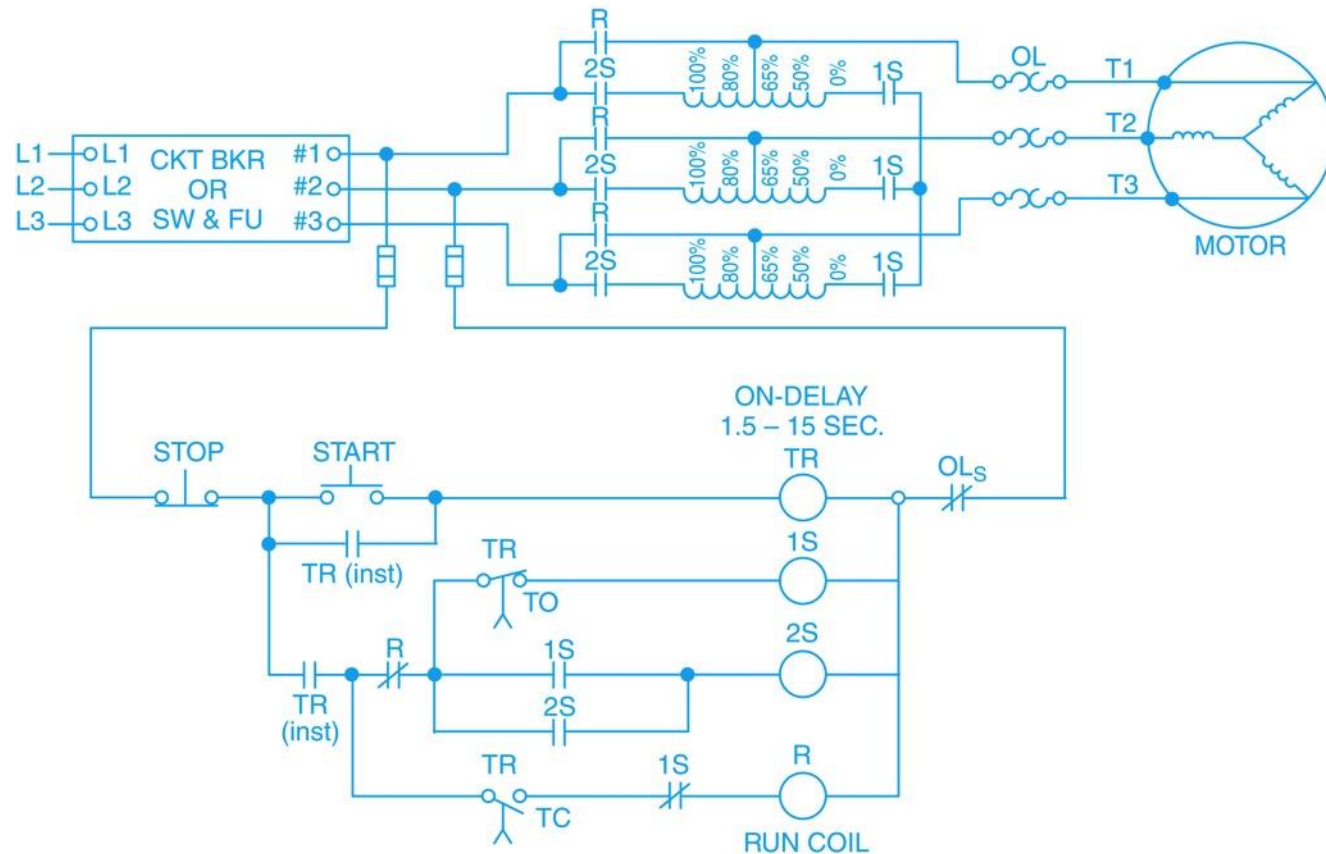
Reduced-Voltage Starting Motor Control

- Autotransformer reduced-voltage starting circuits allow for adjustment of the starting torque and inrush current to help accelerate the load.
- Autotransformers are typically used with high-torque loads such as reciprocating compressors, grinding mills, and pumps.



5.0.0 – 5.5.0

Typical Autotransformer Reduced-Voltage Starting Circuit



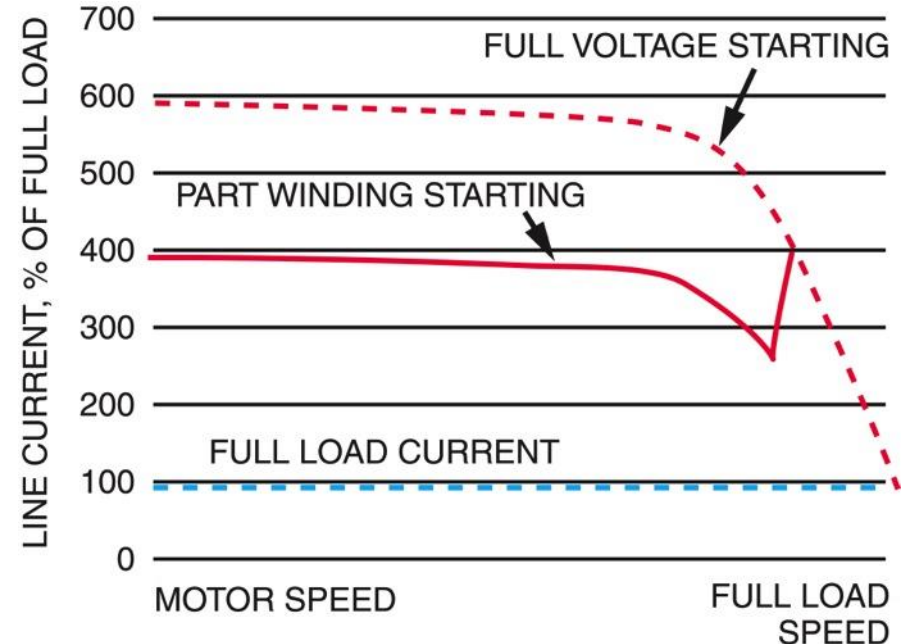
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5.0.0 – 5.5.0

Part-Winding, Reduced-Voltage Starting Characteristics

- Part-winding, reduced-voltage starting motor control is an older method of motor control used with part-winding induction motors.
- The induction motor is started by applying power to part of the motor's coil windings for starting, then the remaining windings for normal running.



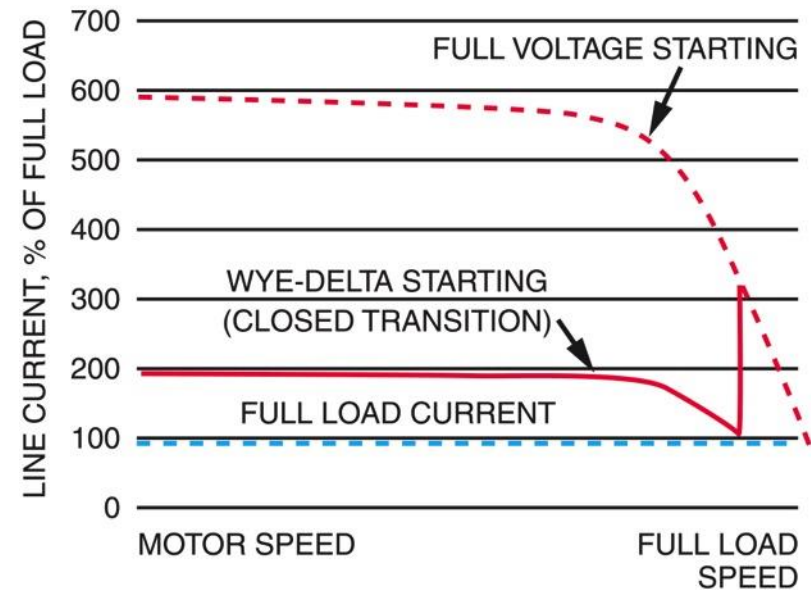
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5.0.0 – 5.5.0

Wye-Delta, Reduced-Voltage Starting Characteristics

- Wye-delta, reduced-voltage starting operates by first connecting the leads in a wye configuration for starting, then connecting them in a delta configuration for running.
- Wye-delta starters are used to control high-inertia loads with long acceleration times, such as centrifugal compressors, centrifuges, and similar loads.

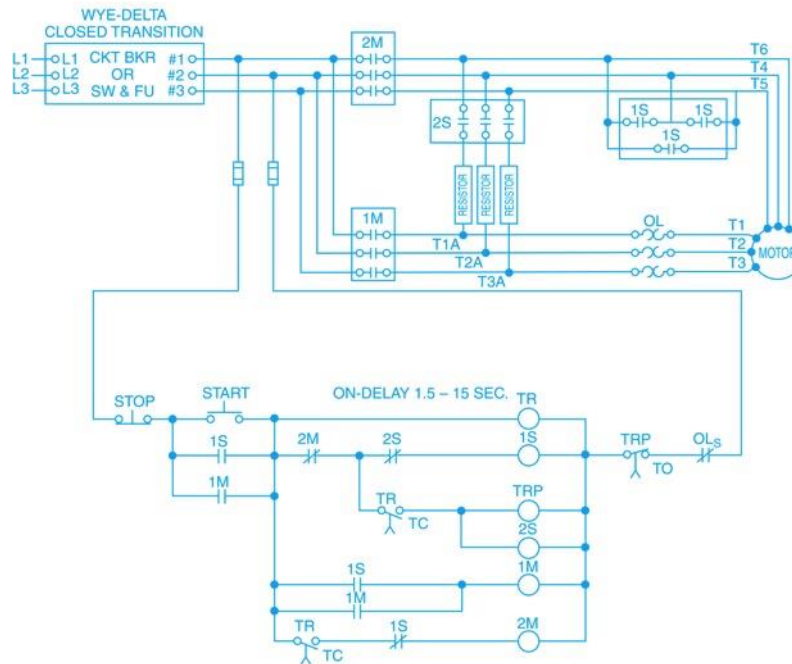
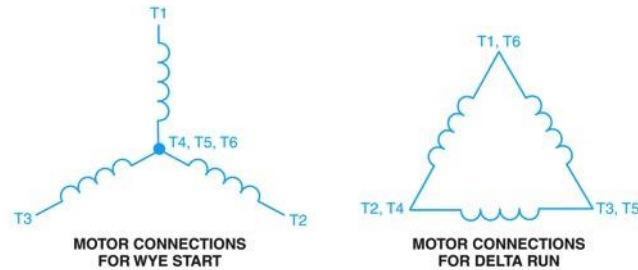


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5.0.0 – 5.5.0

Typical Wye-Delta, Reduced-Voltage Starting Circuit



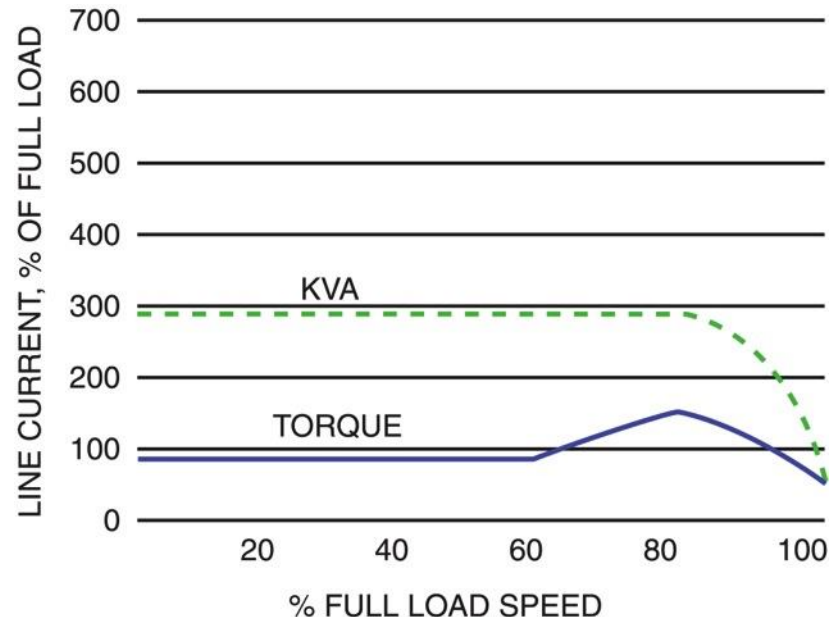
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5.0.0 – 5.5.0

Solid-State, Reduced-Voltage Starting Characteristics

- Solid-state, reduced-voltage starters provide the same functions as electromechanical starters but supply a smoother start/acceleration. They are often referred to as soft-start controllers.
- Soft-start controllers are used with conveyors, compressors, and pumps.

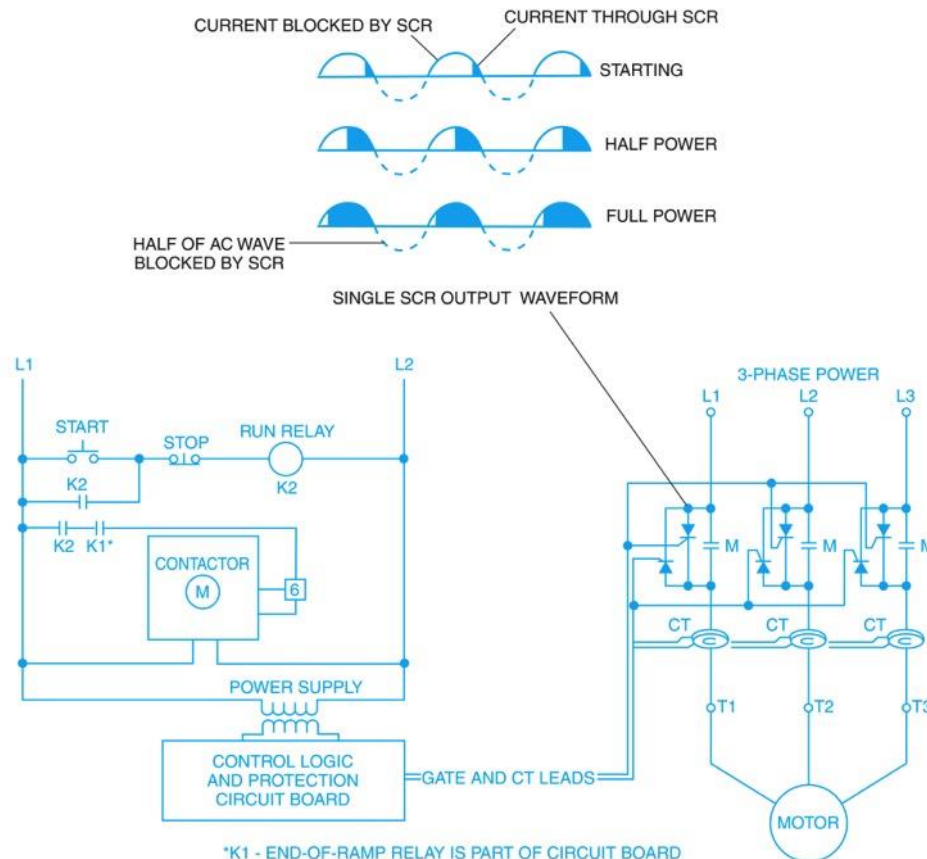


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5.0.0 – 5.5.0

Simplified Solid-State, Reduced-Voltage Starting Circuit

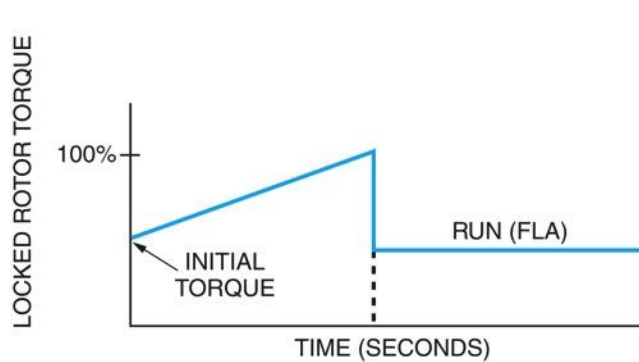


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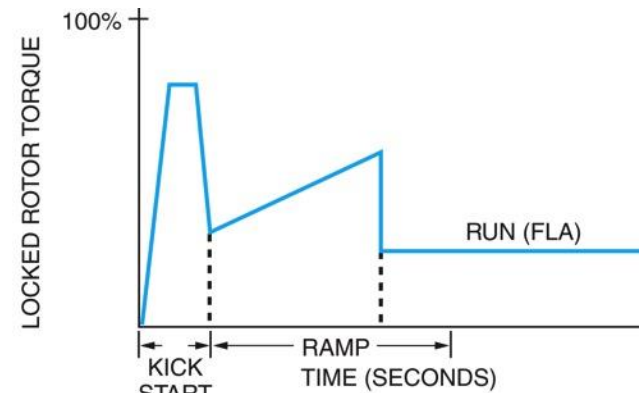


5.0.0 – 5.5.0

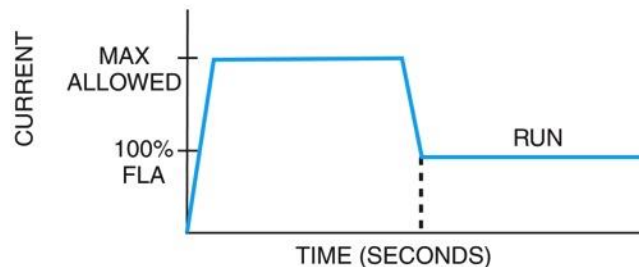
Starting Characteristics of Solid-State, Reduced-Voltage Controllers



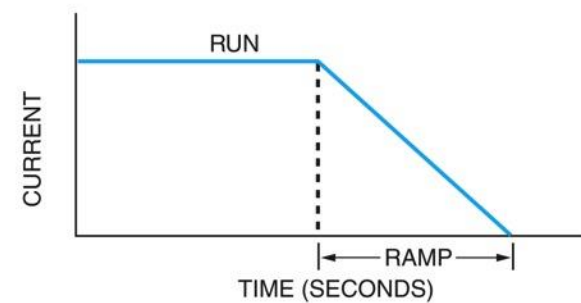
(A) RAMP START



(B) KICK START



(C) CURRENT LIMIT



(D) SOFT STOP

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5.0.0 – 5.5.0

Comparison of Reduced-Voltage Controllers

Type of Reduced-Voltage Controller	Starting Characteristics			Remarks
	Voltage at Motor (%)	Line Current (%)	Torque (%)	
Autotransformer	80	64	64	<i>Applications</i> —Blowers, pumps, compressors, conveyors
	65	42	42	
	50	25	25	

Advantages

- Provides maximum torque per ampere of line current
- Starting characteristics easily adjusted
- Different starting torques available through auto-transformer taps
- Suitable for relatively long starting periods
- Motor current greater than line current during starting

Disadvantages

- Most complex of reduced-voltage controllers because proper sequencing of energization must be maintained
- Large physical size
- Low power factor
- Expensive in lower hp ratings



5.0.0 – 5.5.0

Next Session... of Reduced-Voltage Controllers

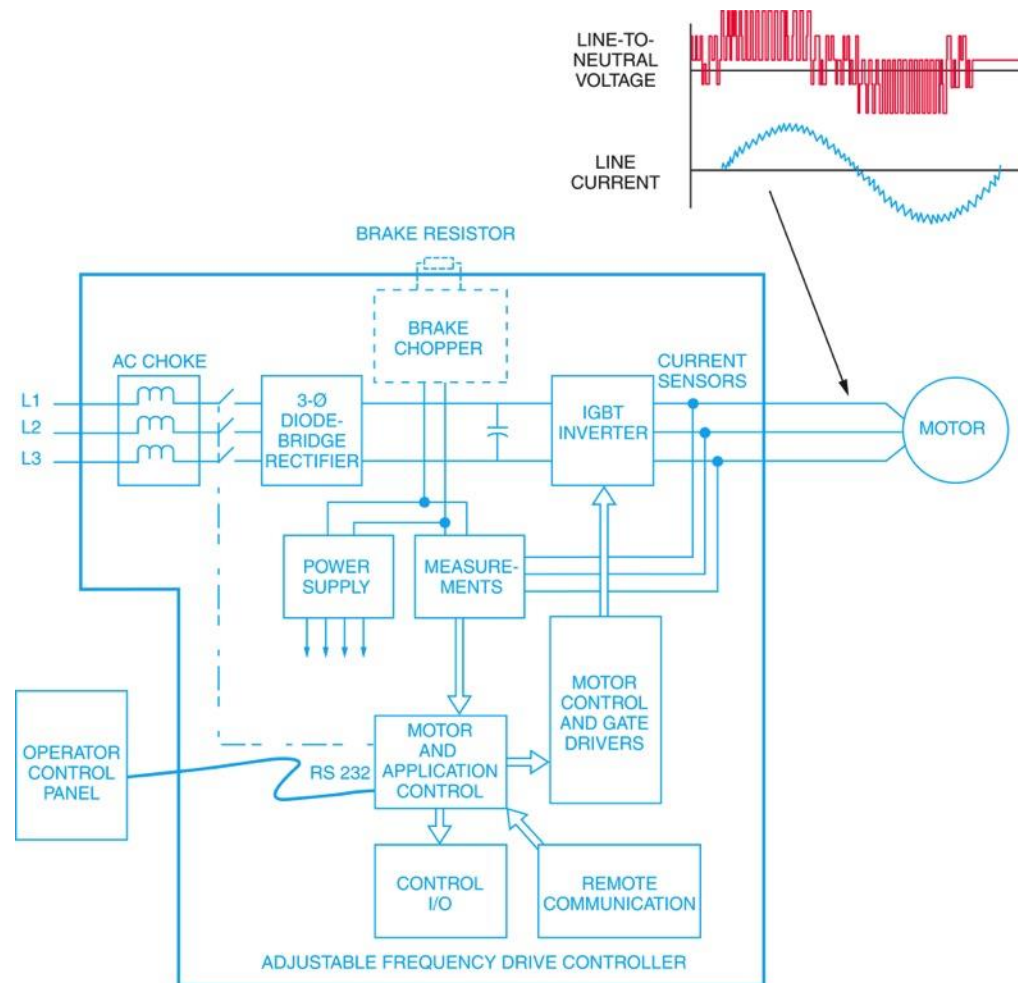
Adjustable Frequency Drives

Type of Reduced-Voltage Controller	Starting Characteristics			Remarks
	Voltage at Motor (%)	Line Current (%)	Torque (%)	
Part-winding	100	65	48	<p>Applications—Reciprocating compressors, pumps, blowers, fans</p> <p><i>Advantages</i></p> <ul style="list-style-type: none">• Least expensive• Small physical size• Suitable for low or high voltage• Full acceleration in one step for most standard induction or special part-winding motors when $\frac{2}{3}$ winding connection is used <p><i>Disadvantages</i></p> <ul style="list-style-type: none">• Unsuitable for high-inertia loads• Specific motor types required• Motor does not start when torque required by load exceeds that developed by motor when first winding is energized
Wye-delta	100	33	33	<p>Applications—Centrifugal compressors, centrifuges</p> <p><i>Advantages</i></p> <ul style="list-style-type: none">• Suitable for high-inertia, long-accelerating loads• High torque efficiency• Ideal for stringent inrush current restrictions• Ideal for frequent starts <p><i>Disadvantages</i></p> <ul style="list-style-type: none">• Requires special motor• Low starting torque• Momentary inrush occurs during open transition when delta contactor is closed (open circuit transition models)
Solid-state	Adjustable	Adjustable	Adjustable	<p>Applications—Machine tools, hoists, packaging equipment, conveyor systems</p> <p><i>Advantages</i></p> <ul style="list-style-type: none">• Voltage gradually applied during starting for a soft-start condition• Adjustable acceleration time• Adjustable kick start, current limit, soft stop <p><i>Disadvantages</i></p> <ul style="list-style-type: none">• More expensive than electromechanical models• Requires specialized installation and maintenance• Electrical transients can damage solid-state components• Requires good ventilation



6.0.0 – 6.5.5

Adjustable Frequency Drives



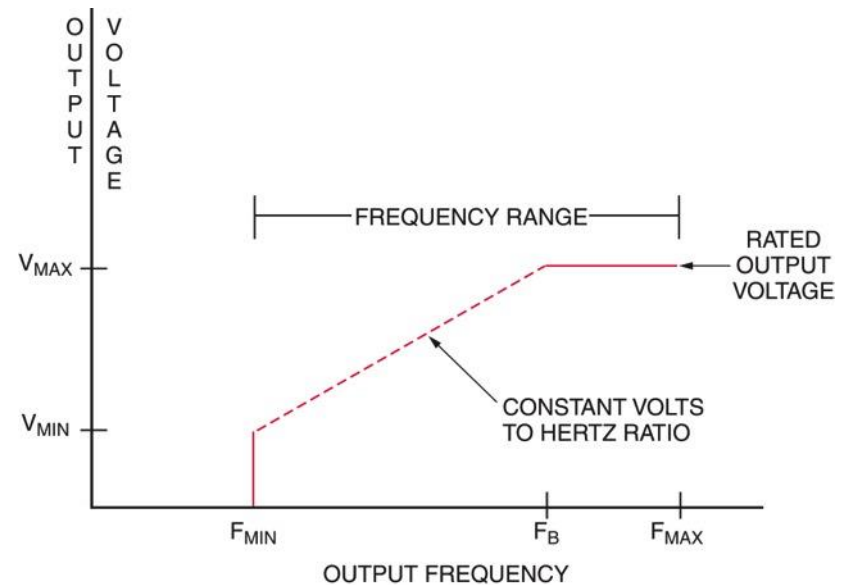
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6.0.0 – 6.5.5

AFD Operating Frequency Range

- AFDs usually have one range of output frequencies over which the ratio of volts to hertz remains constant and another range of output frequencies over which the voltage remains constant but the frequency varies.
- The frequency at which this transition occurs is known as the base frequency.



V_{MIN} = MINIMUM OUTPUT VOLTAGE
 V_{MAX} = MAXIMUM OUTPUT VOLTAGE
 F_{MIN} = MINIMUM FREQUENCY
 F_{MAX} = MAXIMUM FREQUENCY
 F_B = BASE FREQUENCY

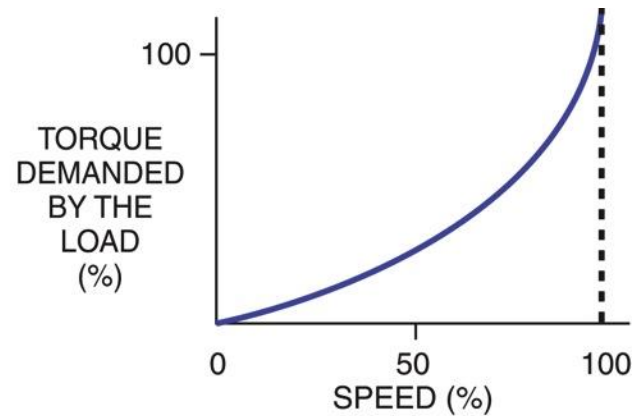
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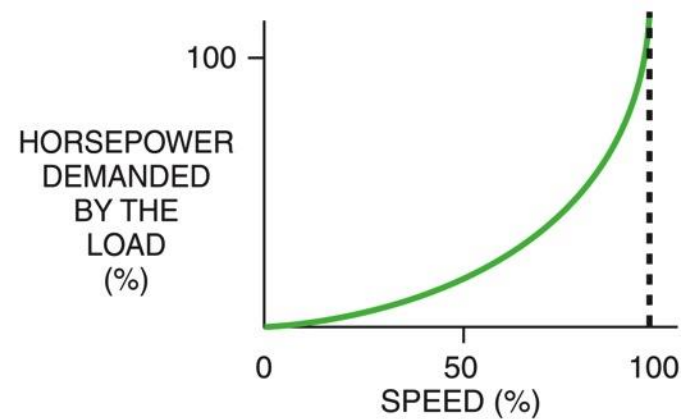
6.0.0 – 6.5.5

Variable Torque Load

- A variable torque load requires a much lower torque at low speeds.
- This type of load is found in machines with high-inertia loads, such as those with flywheels, centrifugal fans, pumps, blowers, and punch presses.



(A)



(B)

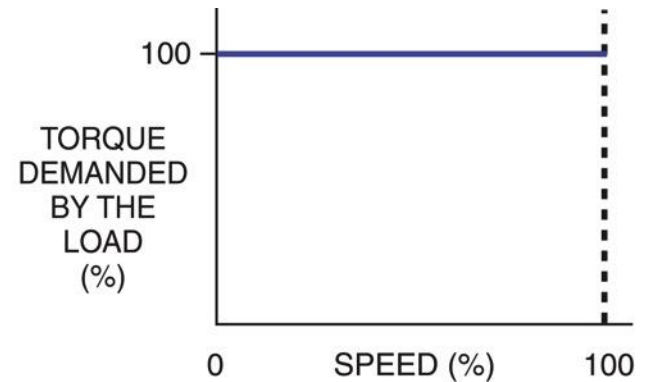
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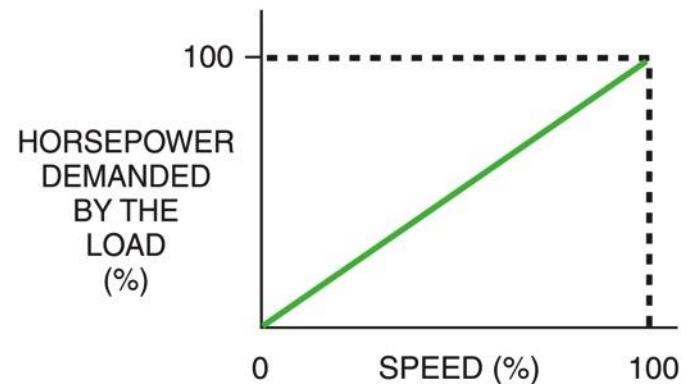
6.0.0 – 6.5.5

Constant Torque Load

- Constant torque loads require high torque to overcome friction. These loads require the same amount of torque at all speeds.
- This type of load is found in hoists, conveyors, printing presses, positive displacement pumps, and extruders, as well as for shock loads, overloads, and high-inertia loads.



(A)



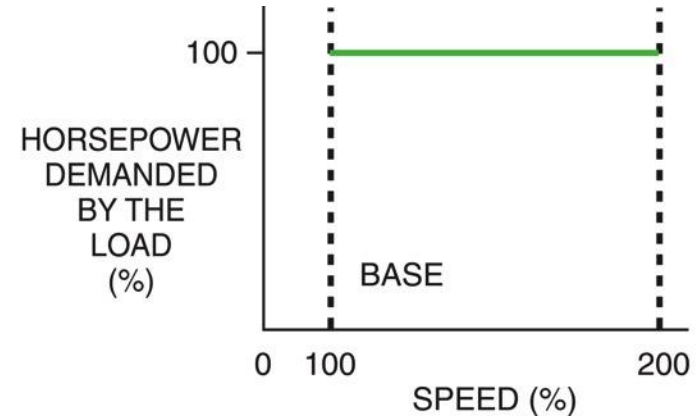
(B)

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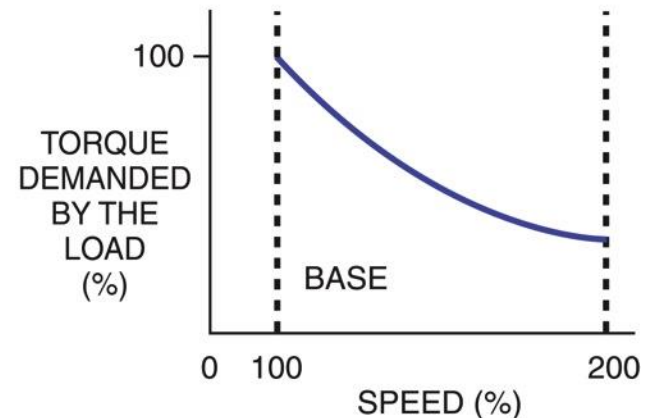
6.0.0 – 6.5.5

Constant Horsepower Load

- Constant horsepower loads require constant horsepower at all speeds.
- This type of load is found in multi-speed metal cutting equipment, mixers, center-driven winders, and some extruders.



(A)



(B)

26407-14_F25.EPS



AFD Application Checklist

AFD APPLICATION CHECKLIST	
Motor	
New _____	Existing _____
Horsepower: _____	Base Speed: _____
Voltage: _____	FLA: _____
LRA: _____	NEMA Design: _____
Gearbox/Pulley Ratio: _____	Service Factor: _____
Load	
Application: _____	
Load Type: Constant Torque _____	Variable Torque _____
Constant Horsepower _____	Load inertia reflected to motor: _____
Required breakaway torque from motor: _____	Running load on motor: _____
Peak torques (above 100% running): _____	Shortest/longest required accel. time: _____ / _____ secs up to _____ Hz from zero speed
Shortest/longest required decel. time: _____ / _____ secs down to _____ Hz from max. speed	Operating speed range: _____ Hz to _____ Hz
Time for motor/load to coast to stop: _____ secs	
AFD	
Source of start/stop commands: _____	
Source of speed adjustment: _____	
Other operating requirements: _____	
Will the motor ever be spinning when the AFD is started? _____	
Is the load considered to be high inertia? _____	
Is the load considered to be hard to start? _____	
Distance from AFD to the motor: _____ feet	
Type of AFD (V/Hz, Flux Vector, Closed Loop Vector): _____	
Options desired: _____	

Other special requirements/conditions: _____	

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6.0.0 – 6.5.5

Next Session... Application Checklist

AFD APPLICATION CHECKLIST (Continued)

Power Supply

Supply Transformer: _____ kVA and _____ % Z or short circuit current at drive input: _____ amps

(If the drive does not include a built-in line reactor and the available feeder short circuit current is more than 100 times the drive FLA rating, a 1% line reactor or a drive isolation transformer is required.)

Total horsepower of all drives connected to supply transformer or feeder: _____ hp

Is a drive transformer or line reactor desired? _____

Any harmonic requirements? _____ % Voltage THD: _____ % Current THD: _____ IEEE 519: _____

Total non-drive load connected to the same feeder as drive(s): _____ amps

Service

Start-up Assistance: _____ Customer Training: _____

Does the AFD operate more than one motor? _____

Will the power supply source ever be switched with the AFD running? _____

Is starting or stopping time critical? _____

Are there any peak torques or impact loads? _____

Will user-supplied contactors be used on the input or output of the AFD? _____

Does the user or utility system have PF capacitors that are being switched? _____

Will the AFD be in a harsh environment or high altitude? _____

Does the utility system experience surges, spikes, or other fluctuations? _____

Motor Braking Methods

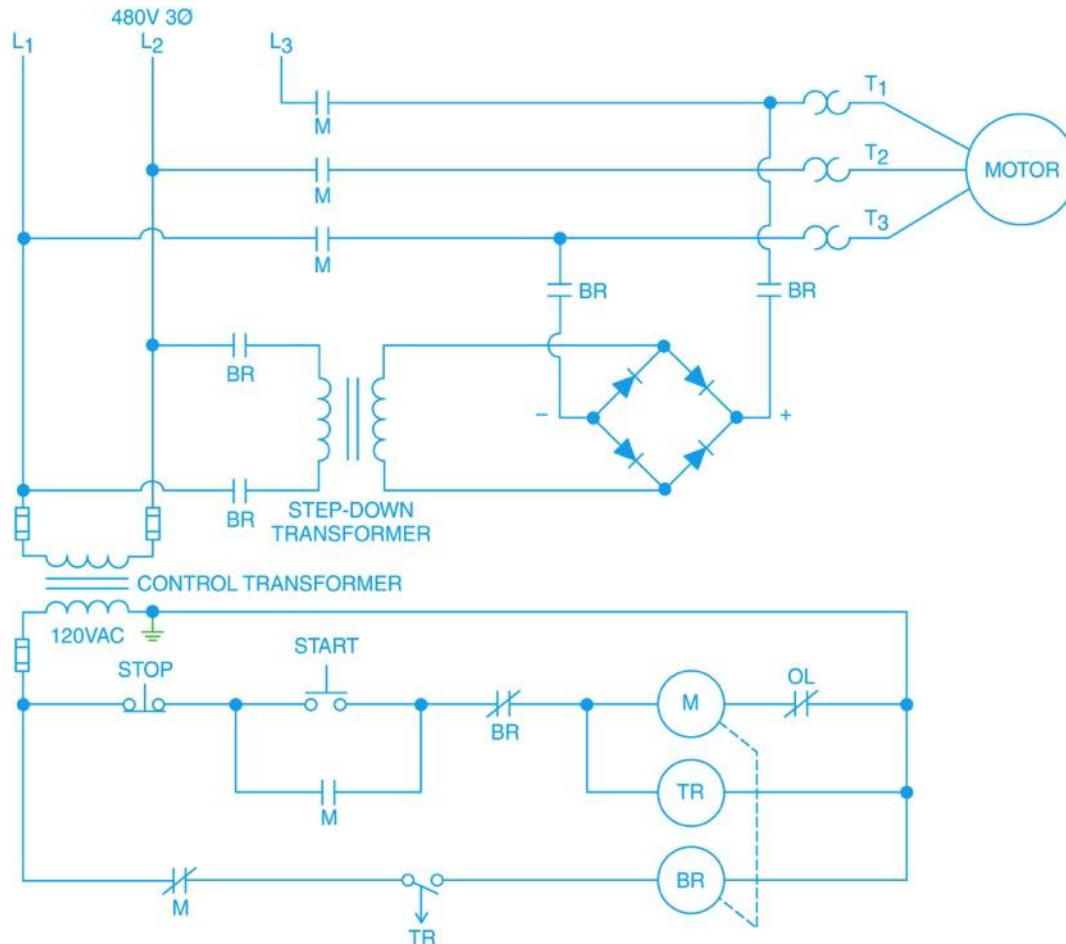
Performance Task

This session will conclude with trainees identifying and connecting various control devices.



7.0.0 – 7.3.0

Motor Braking Methods



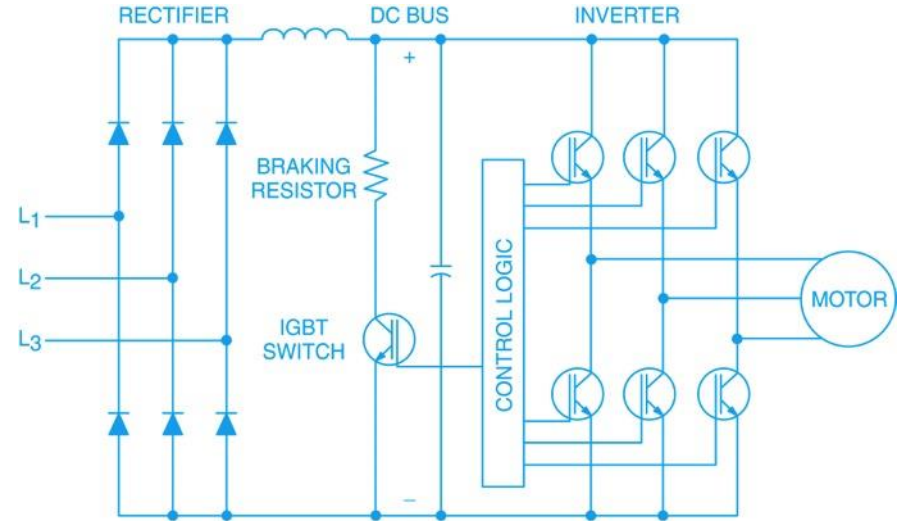
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7.0.0 – 7.3.0

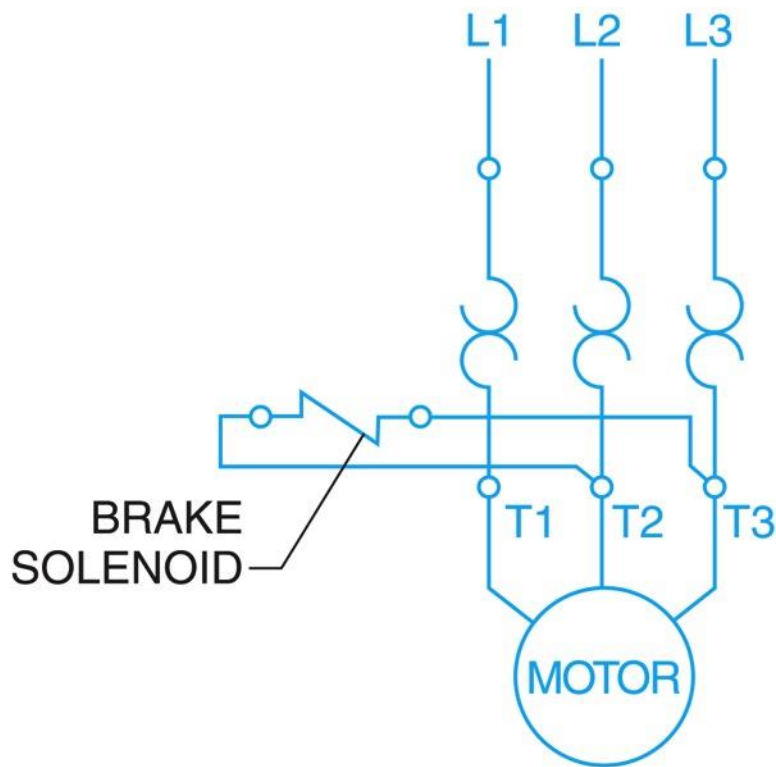
Simplified Schematic of an AC Drive Using Dynamic Braking

- In an AC drive unit, the electrical energy returned by the motor can cause an increase in the voltage to the DC bus, possibly resulting in damage to the drive components.
- A braking resistor can be used to dissipate this excess energy, as shown here.



26407-14_F28.EPS

Friction Brake Solenoid Connection



26407-14_F29.EPS

- Motor braking can also be accomplished using solenoid-operated friction brakes similar to those used on vehicles.
- The solenoid is energized while the motor is running, moving the brake shoes/pads away from the wheel. When the motor is de-energized, the brake shoes/pads contact the wheel to provide friction braking.

7.0.0 – 7.3.0

Next Session... Precautions When Working with Solid-State Controls

- Solid-state equipment is very sensitive and easily damaged by reversed polarity, excess heat, and electrostatic discharge.
- Always ground yourself before handling a circuit board and wear a grounding strap if supplied. Store unused boards in a shielding bag or conductive tote box.

Motor Control Maintenance; Motor Control Troubleshooting



METALLIZED
SHIELDING BAG



CONDUCTIVE
TOTE BOX

26407-14_F30.EPS

9.0.0 – 10.6.8

Motor Control Maintenance; Motor Control Troubleshooting

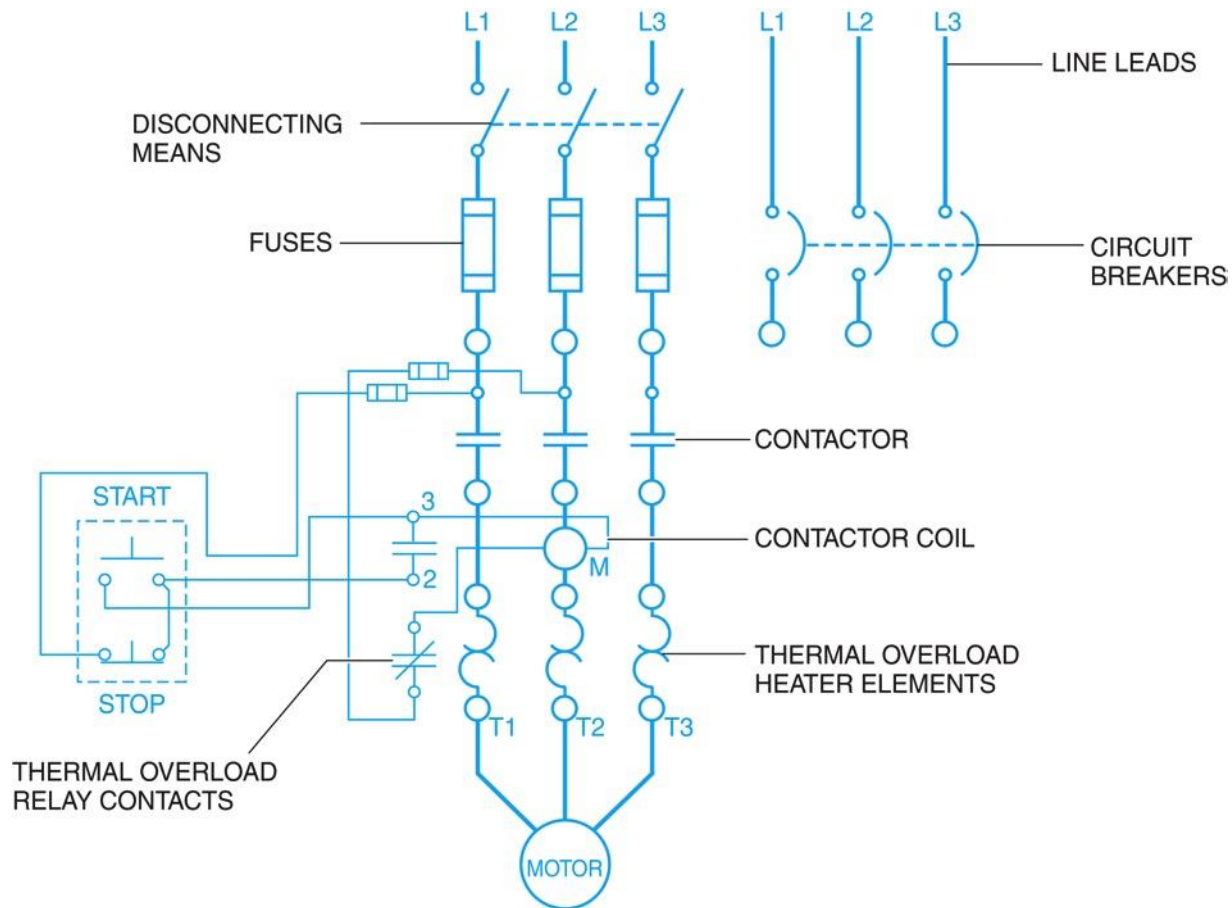
FAULT CODES	FAULT	POSSIBLE CAUSES	CHECKING
F1	OVERCURRENT	FREQUENCY CONVERTER HAS MEASURED TOO HIGH A CURRENT IN THE MOTOR OUTPUT: – SUDDEN HEAVY LOAD INCREASE – SHORT CIRCUIT IN THE MOTOR CABLES – UNSUITABLE MOTOR	CHECK THE LOAD CHECK THE MOTOR SIZE CHECK THE CABLES
F2	OVERVOLTAGE	THE VOLTAGE OF THE INTERNAL DC-LINK OF THE FREQUENCY CONVERTER HAS EXCEEDED THE NOMINAL VOLTAGE BY 35%: – DECELERATION TIME IS TOO FAST – HIGH OVERVOLTAGE SPIKES AT UTILITY	ADJUST THE DECELERATION TIME
F3	GROUND FAULT	CURRENT MEASUREMENT HAS DETECTED THAT THE SUM OF THE MOTOR PHASE CURRENT IS NOT ZERO: – INSULATION FAILURE IN THE MOTOR OR THE CABLES	CHECK THE MOTOR CABLES
F4	INVERTER FAULT	FREQUENCY CONVERTER HAS DETECTED FAULTY OPERATION IN THE GATE DRIVERS OR IGBT BRIDGE: – INTERFERENCE FAULT – COMPONENT FAILURE	RESET THE FAULT AND RESTART AGAIN; IF THE FAULT OCCURS AGAIN, CONTACT YOUR DISTRIBUTOR
F5	CHARGING SWITCH	CHARGING SWITCH IS OPEN WHEN THE START COMMAND IS ACTIVE: – INTERFERENCE FAULT – COMPONENT FAILURE	RESET THE FAULT AND RESTART AGAIN; IF THE FAULT OCCURS AGAIN, CONTACT YOUR DISTRIBUTOR
F6	UNDERVOLTAGE	DC-BUS VOLTAGE HAS GONE BELOW 65% OF THE NOMINAL VOLTAGE: – MOST COMMON REASON IS FAILURE OF THE UTILITY SUPPLY	IN CASE OF TEMPORARY SUPPLY VOLTAGE BREAK, RESET THE FAULT AND RESTART

26407-14_F31.EPS



9.0.0 – 10.6.8

Basic Motor Control Circuit



26407-14_F32.EPS



9.0.0 – 10.6.8

Motor Control Troubleshooting Chart

Malfunction	Possible Cause	Corrective Action
Constant chatter	Broken pole shaver Poor contact in control circuit Low voltage	Replace. Improve contact or use holding circuit interlock (three-wire control). Correct voltage condition; check momentary voltage dip during starting.
Contactors welding or freezing	Abnormal inrush of current Rapid jogging Insufficient contact pressure Low voltage preventing magnet from sealing Foreign matter preventing contacts from closing Short circuit	Use larger contactor or check for grounds. Install larger device rated for jogging service. Replace contact springs; check contact carrier for damage. Correct voltage condition; check momentary voltage dip during starting. Clean contacts with approved solvent. Remove fault and check to be sure fuse or breaker size is correct.
Short contact life or tip overheating	Filing or dressing Interrupt excessively high Excessive jogging Weak contact pressure Dirt or foreign matter on contact surface Short circuit Loose connection Sustained overload	Do not file silver-faced contacts; rough spots or discoloration will not harm contacts. Install larger device or check currents for grounds, shorts, or excessive motor currents; use silver-faced contacts. Install larger device rated for jogging. Adjust or replace contact springs. Clean contacts with approved solvent. Remove fault and check for proper fuse or breaker size. Clean and tighten. Install larger device or check for excessive load current.
Coil overheating	Overvoltage or high ambient temperature Incorrect coil Shorted turns caused by mechanical damage or corrosion Undervoltage, failure of magnet to seal in Dirt or rust on pole faces increasing air gap	Check application and circuit. Check rating and if incorrect, replace with proper coil. Replace coil. Correct system voltage. Clean pole faces.
Overload relays tripping	Sustained overload Loose connection on load wires Incorrect heater	Check for grounds, shorts, or excessive currents. Clean and tighten. Replace relay with correct size heater unit.
Failure to trip causing motor burnout	Mechanical binding, dirt, corrosion, etc. Wrong heater or heaters omitted and jumper wires used Motor and relay at different temperatures Wrong calibration or improper calibration adjustment	Clean or replace. Check ratings; apply proper heater. Adjust relay rating accordingly. Consult factory.
Magnetic and mechanical parts inoperative	Broken shading coil	Replace shading coil.
Noisy magnet humming	Magnet faces not mating Dirt or rust on magnet faces Low voltage	Replace magnet assembly; realign. Clean and realign. Check system voltage and voltage dips during starting.
Failure to pick up and seal	Low voltage Coil open or shorted Wrong coil Mechanical obstruction	Check system voltage and voltage dips during starting. Replace. Check coil number. With power off, check for free movement of contact and armature assembly.



9.0.0 – 10.6.8

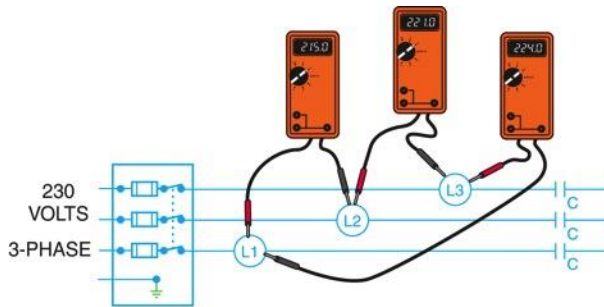
Motor Control Troubleshooting Chart

Malfunction	Possible Cause	Corrective Action
Failure to drop out	Gummy substance on pole faces Voltage not removed Worn or rusted parts causing binding Residual magnetism due to lack of air gap in magnet path	Clean with solvent. Check coil circuit. Replace parts. Replace worn magnet parts.



9.0.0 – 10.6.8

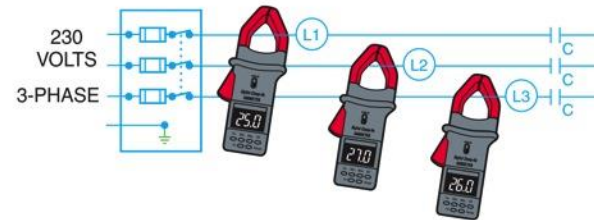
Three-Phase Input Voltage Checks



- | 1) PHASE | MEASURED READING |
|----------|------------------|
| L1 | 215V |
| L2 | 221V |
| L3 | 224V |
- 2) AVERAGE VOLTAGE = $\frac{215 + 221 + 224}{3} = 220V$
- 3) INDIVIDUAL PHASE UNBALANCE FROM AVERAGE } L1 TO L2 = 220 - 215 = 5V
 L2 TO L3 = 221 - 220 = 1V
 L3 TO L1 = 224 - 220 = 4V
- 4) 5V = MAXIMUM UNBALANCE
- 5) % UNBALANCE = $\frac{\text{MAXIMUM UNBALANCE}}{\text{AVERAGE VOLTAGE}} \times 100$
 % UNBALANCE = $\frac{5V}{220V} \times 100 = 2.27\%$ (OUT OF BALANCE)

MAXIMUM VOLTAGE UNBALANCE BETWEEN ANY TWO LEGS MUST NOT EXCEED 2%.

(A) CALCULATING VOLTAGE UNBALANCE



- | 1) PHASE | MEASURED READING |
|----------|------------------|
| L1 | 25A |
| L2 | 27A |
| L3 | 26A |
- 2) AVERAGE CURRENT = $\frac{25 + 27 + 26}{3} = 26A$
- 3) INDIVIDUAL PHASE UNBALANCE FROM AVERAGE } L1 TO L2 = 25 - 27 = 2A
 L2 TO L3 = 27 - 26 = 1A
 L3 TO L1 = 26 - 25 = 1A
- 4) 2A = MAXIMUM UNBALANCE
- 5) % UNBALANCE = $\frac{\text{MAXIMUM UNBALANCE}}{\text{AVERAGE CURRENT}} \times 100$
 % UNBALANCE = $\frac{2A}{26A} \times 100 = 7.7\%$ (IN BALANCE)

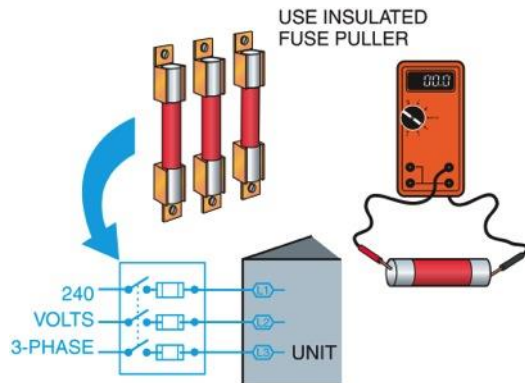
MAXIMUM CURRENT UNBALANCE BETWEEN ANY TWO LEGS MUST NOT EXCEED 10%.

(B) CALCULATING CURRENT UNBALANCE

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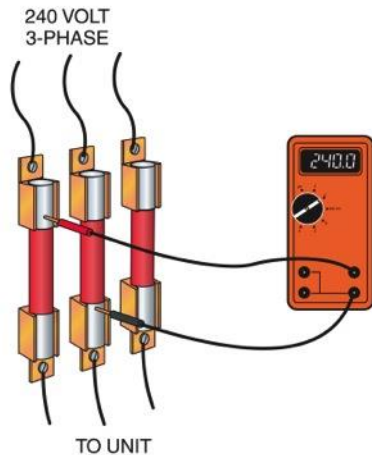


9.0.0 – 10.6.8



ZERO Ω READING = GOOD FUSE
MEASURABLE OR INFINITE RESISTANCE READING = BAD FUSE

CONTINUITY CHECK



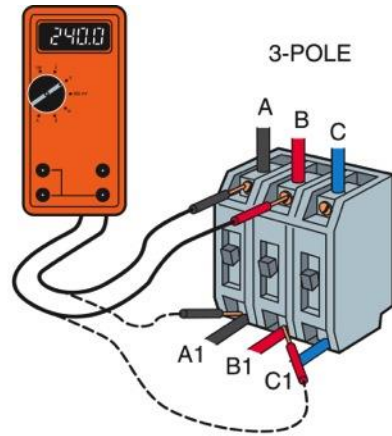
VOLTAGE CHECK

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Fuse Checks

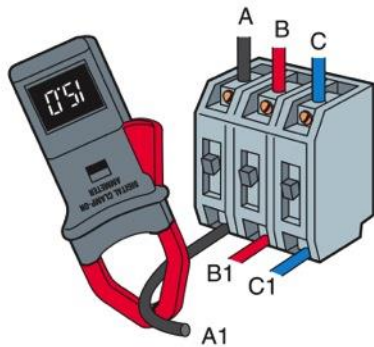
- Fuses and circuit breakers are normally the first items checked when a motor is inoperative.
- One way to test a fuse is by measuring continuity using a VOM/DMM. If the fuse shows zero ohms, it is usually good. A blown fuse will indicate infinite resistance.

9.0.0 – 10.6.8



MEASURED INPUT AND OUTPUT VOLTAGES SHOULD BE THE SAME.

CIRCUIT BREAKER VOLTAGE CHECK



CIRCUIT BREAKER CURRENT CHECK

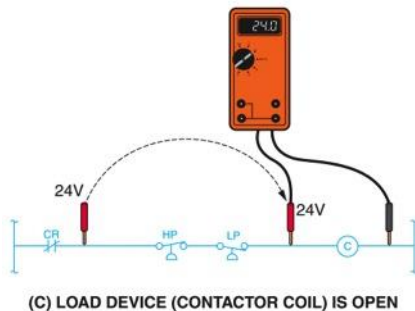
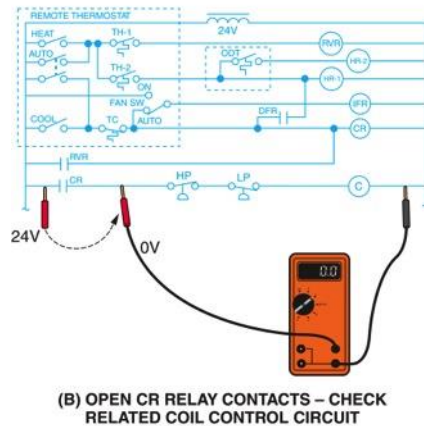
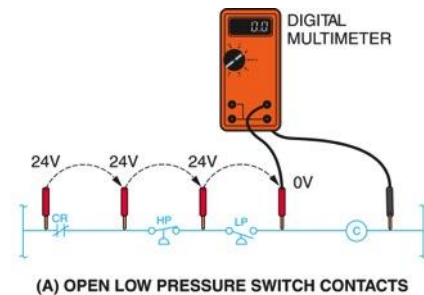
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Circuit Breaker Checks

- To test a circuit breaker, measure the voltage between A1 to B1, B1 to C1, and C1 to A1. A good breaker will show equal voltages on all input and output terminals.
- If a circuit breaker is overheating, measure the current at A1, B1, and C1. A breaker that trips at a current below its rating or is not tripping at a higher current should be replaced.

9.0.0 – 10.6.8

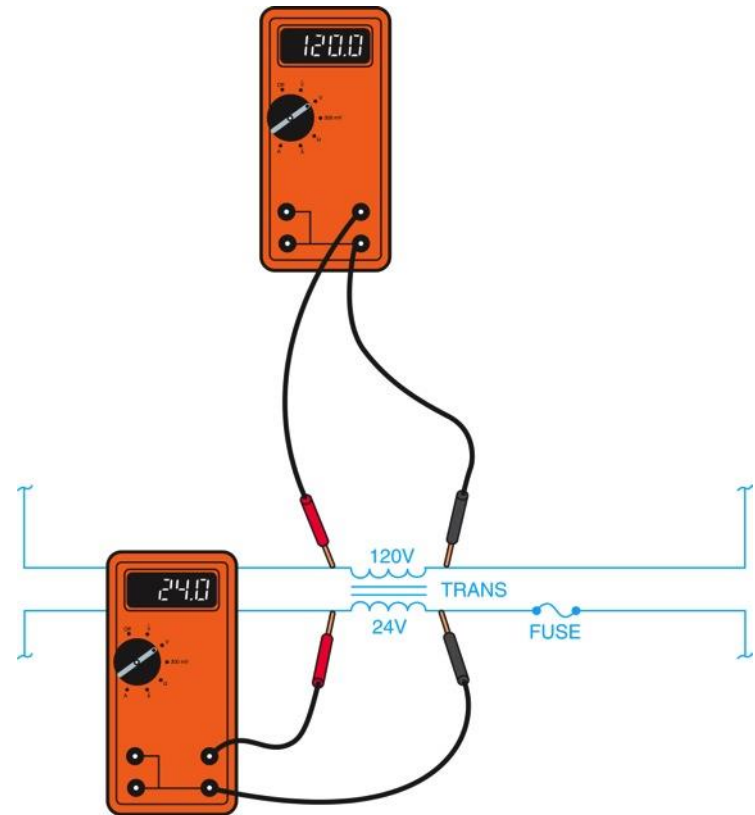
Isolating a Faulty Control Circuit Component



- A series of voltage measurements can be made across each device in a control circuit to locate a faulty device.
- Start from the line or control voltage side and move toward the load side. If a zero reading is found, there is an open set of contacts between the last two measurement points.

Control Transformer Checks

- Control transformers can be checked by measuring the voltage across the primary and secondary windings.
- The secondary winding is usually measured first. If it is within 10% of the required voltage, the transformer is good.

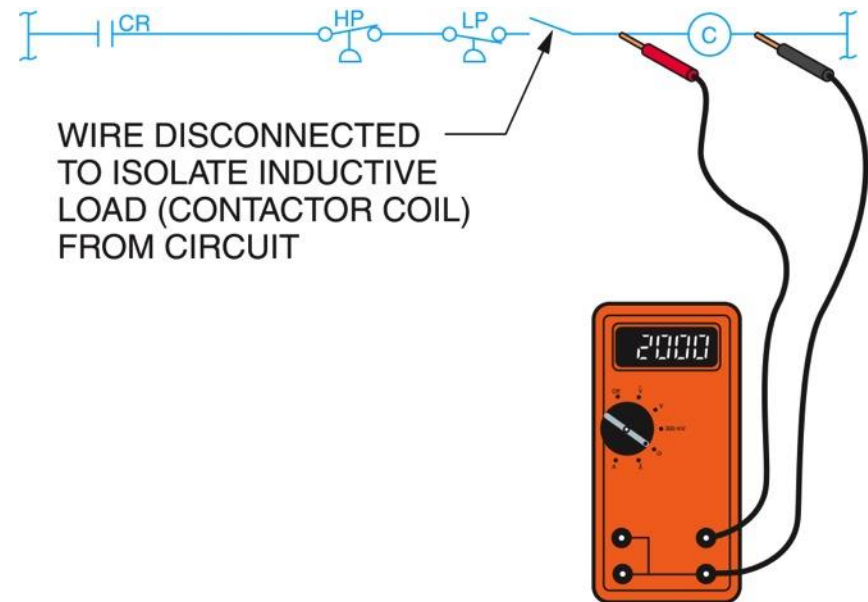


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9.0.0 – 10.6.8

Coil Resistance Checks

- The best way to test a coil is to electrically isolate the coil and then measure the resistance across its terminals.
- A reading of zero ohms indicates a shorted coil and a reading of infinite resistance indicates an open coil.



MEASURABLE RESISTANCE = GOOD LOAD
ZERO RESISTANCE = SHORTED LOAD
INFINITE RESISTANCE = OPEN LOAD

26407-14_F38.EPS

9.0.0 – 10.6.8

Next Session... Checking the Continuity of Contactor/Relay Contacts

- With power to the circuit turned off, contacts can be tested by making a continuity measurement to determine whether the contacts are open or closed.
- If the contacts are open, the VOM/DMM will show a reading of infinite resistance.

Wrap Up



ZERO OHMS =
CLOSED CONTACTS



INFINITE RESISTANCE =
OPEN CONTACTS

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Wrap Up

3-2-1

- 3 – Write 3 important things learned during class
- 2 – Write 2 questions you have about the material
- 1 – Write 1 thought you had about the material



Next Session...

MODULE EXAM

Review the complete module to prepare for the module exam. Complete the Module Review as a study aid.

